

Turbulence Closure, Scales, and Similarity Theory

Review Terms

- Statically stable
- Dynamically unstable
- Isotropic / anisotropic
- Turbulence tends to homogenize

“Unstable” profiles

- How does one even get an unstable potential temperature profile?
 - Because of outer space
 - Radiative – Convective (Dis)Equilibria
- What profiles of wind velocity (shear) produce turbulence?
 - On the board
- Richardson # : A balance between mechanical production and buoyant dissipation of turbulence

$$\text{Ri} = \frac{-B}{M} \approx \frac{\frac{g}{\theta_v} \frac{\partial \overline{\theta}_v}{\partial z}}{\left(\frac{\partial \overline{u}}{\partial z}\right)^2 + \left(\frac{\partial \overline{v}}{\partial z}\right)^2}$$

For $\text{Ri} < 0.25$, laminar flow becomes turbulent.

For $\text{Ri} > 1$, turbulent flow becomes laminar.

For $0.25 < \text{Ri} < 1$, the existence of turbulence depends on the flow's history.

9.1.4 Turbulent transport and fluxes

- Kinematic heat flux:

$$\overline{w'\theta'}$$

- For a layer of air:

$$\frac{\partial \overline{\theta}}{\partial t} = - \frac{\partial \overline{w'\theta'}}{\partial z} + \dots$$

9.1.4 Turbulent transport and fluxes

- For a layer of air:

$$\frac{\partial \overline{\theta}}{\partial t} = - \frac{\partial \overline{w' \theta'}}{\partial z} + \dots$$

- The turbulent flux of the heat flux:

$$\frac{\partial \overline{w' \theta'}}{\partial t} = - \frac{\partial \overline{w' w' \theta'}}{\partial z} + \dots$$

9.1.4 Turbulent transport and fluxes

- This is the turbulence closure problem
 - Make a “closure assumption”
 - Can such a parameterization ever be perfect?

9.1.5 Turbulence Closure

- Statistical Order and Non-localness
- An example:
- “Gradient-transfer theory” or “K-theory” or “Eddy-diffusivity theory”

$$F_H = \overline{w'\theta'} = -K \frac{\partial \bar{\theta}}{\partial z}$$

9.1.5 Turbulence Closure

- This is a first-order closure
- K is an “Eddy diffusivity” – work out units on board

$$F_H = \overline{w'\theta'} = -K \frac{\partial \bar{\theta}}{\partial z}$$

Turbulence Closure

- A local closure for K
- Relate to local TKE and a turbulence length scale:

$$K = le,$$

where

$$e = (\sigma_u^2 + \sigma_v^2 + \sigma_w^2)^{1/2}$$

9.1.5 Turbulence Closure

- A local closure for K
 - Related to the local wind shear and a mixing length “ l ”

$$K = l^2 \left| \frac{\partial V}{\partial z} \right|$$

- l is an average eddy size
 - At very low levels (in the surface layer) l can be approximated by kz where $k=0.4$

$$l = (\overline{z'^2})^{1/2}$$

$$l \approx kz$$

9.1.5 Turbulence Closure

- What would a non-local closure for K be?

$$F_H = \overline{w'\theta'} = -K \frac{\partial \bar{\theta}}{\partial z}$$

9.1.6 Scales, scales, scales

- Velocity Scales

❑ Friction velocity:

$$u_* = \left[\overline{u'w'^2} + \overline{v'w'^2} \right]^{\frac{1}{4}} \quad u_*^2 = \left(\overline{u'w'} \right) \quad \text{For one-dimensional case}$$

Friction velocity relevant to statically neutral conditions in the surface layer

❑ Convective velocity scale (Deardorff velocity):

$$w_* = \left[\frac{g \cdot z_i}{T_v} \overline{w'\theta'_s} \right]^{\frac{1}{3}}$$

Deardorff velocity relevant to unstably stratified boundary layer

z_i – height of capping inversion (PBL height)

T_v – virtual temperature

9.1.6 Scales, scales, scales

- Length Scales

- z_i : the altitude of the inversion. Relevant length scale for statically unstable and neutral conditions
- z_0 : the roughness length
- The Obukhov length L
 - For statically non-neutral conditions: This is the height in the surface layer below which mechanical production of turbulence dominates

$$L = \frac{-u_*^3}{k \frac{g}{T_v} (\overline{w'\theta'})_s}$$

9.1.6 Scales, scales, scales

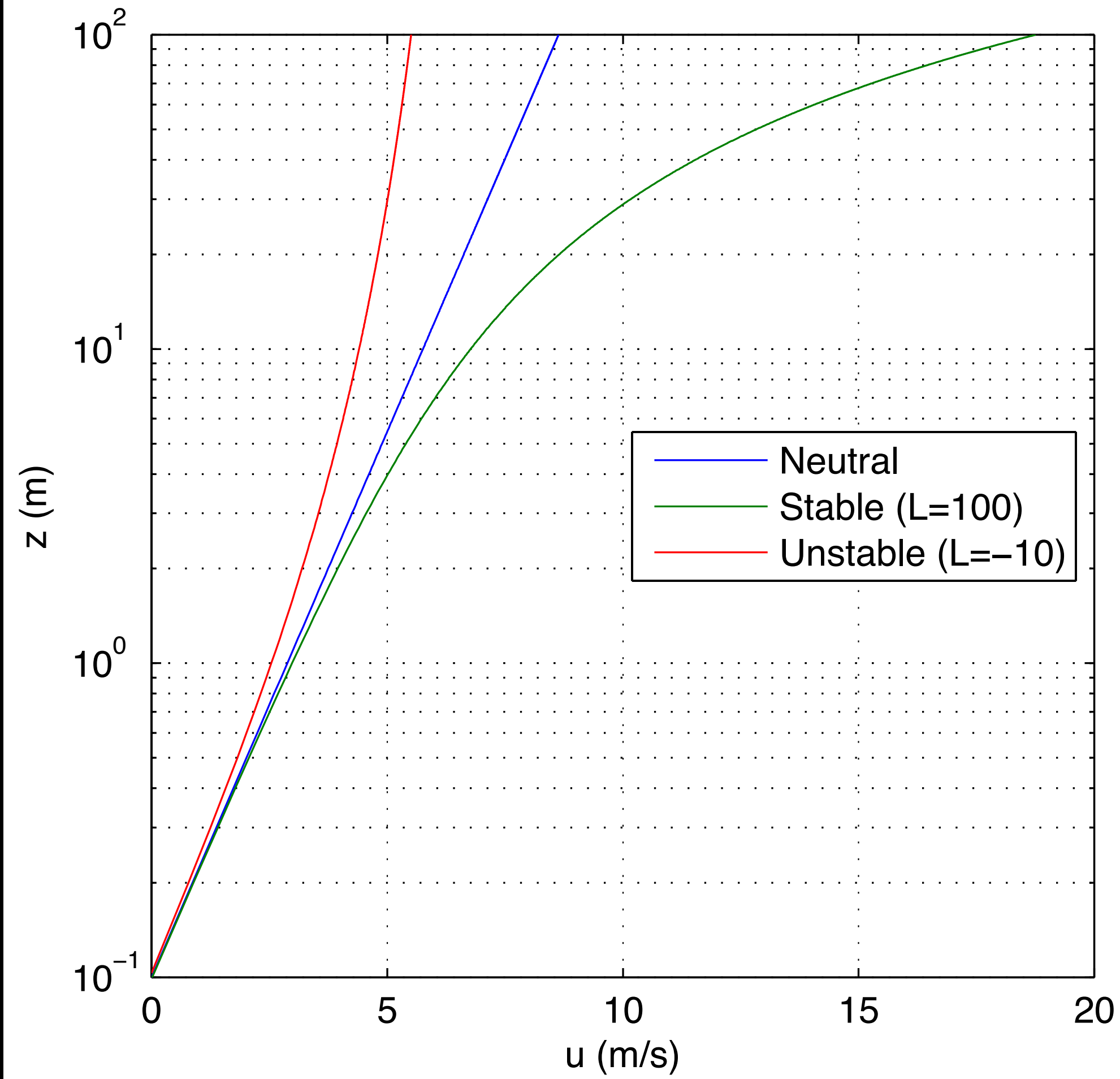
- Length Scales
 - z_0 : the roughness length

$$U(z) = \frac{u_*}{k} \log\left(\frac{z}{z_0}\right)$$

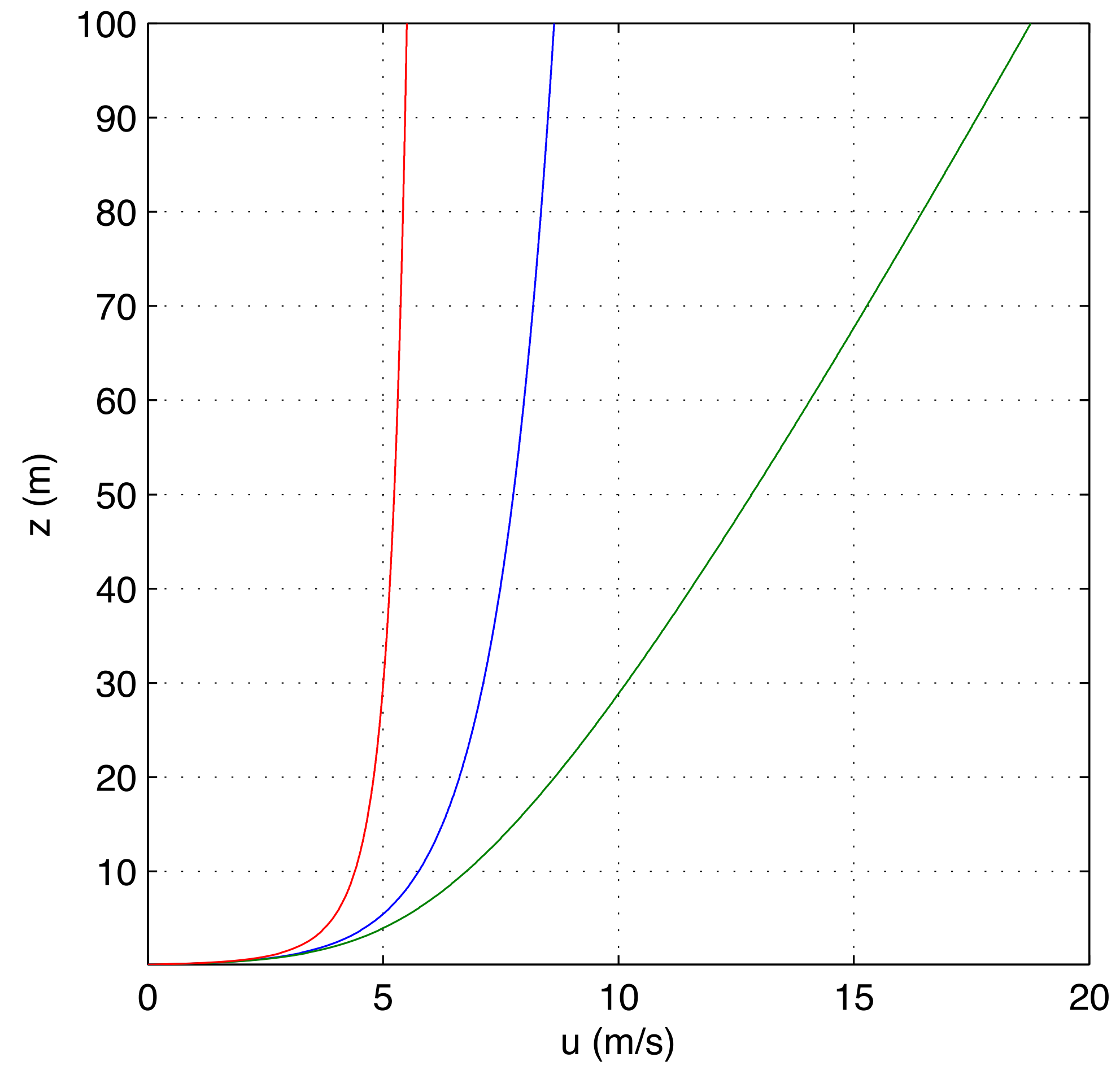
Logarithmic wind profile
valid for **neutral** conditions

10⁻²

HW 4 Problem 2 ($u_*=0.5$)



HW 4 Problem 2 ($u_*=0.5$)



9.1.6 Scales, scales, scales

- Time Scales

- For convective boundary layer (turnover time for largest eddies)

$$t^* = \frac{z_i}{w^*}$$

- For neutral surface layer: (faster times possible)

$$t^*_{SL} = \frac{z}{u^*}$$

9.1.6 Scales, scales, scales

- Summary:
 - For the convective boundary layer
 - w^* and z_i
 - For the surface layer
 - If neutral: u^* and z_0
 - If non-neutral: u^* and z_0 and L

9.1.6 Similarity

- Example: Through the depth of a convective boundary layer:

$$\frac{\overline{w'^2}}{w_*^2} = a \left(\frac{z}{z_i} \right)^b \left(1 - c \frac{z}{z_i} \right)^d$$

- Example: For a statically stable surface layer (compare with neutral log wind profile)

$$\frac{V}{u_*} = 2.5 \left[\ln \left(\frac{z}{z_0} \right) + 8.1 \frac{z}{L} \right]$$