

## Buoyant Plume: Line Source

### Structure: Neutral Stratification

From Rouse, Yih, and Humphreys (1952), via section 2.3 of Emanuel's *Atmospheric Convection*, the vertical velocity in the plume is a function of  $x$  and  $z$ :

$$w(x, z) = 1.8 F^{1/3} \exp\left(-32 \frac{x^2}{z^2}\right),$$

where

$$F = \int_{-\infty}^{+\infty} w b dx,$$

is the integrated (or total) buoyancy flux of the plume and  $x$  is the coordinate normal to the line source.

The buoyancy in the plume is also a function of  $x$  and  $z$ :

$$b(x, z) = 2.6 F^{2/3} z^{-1} \exp\left(-41 \frac{x^2}{z^2}\right),$$

and the plume half-width is

$$R = 0.16z.$$

What is the vertical velocity at  $x = R$ ?

$$\frac{w(R, z)}{w(0, z)} = \exp(-32(0.16)^2) \approx 0.44.$$

The mass flux of a plume per unit length along the line source ( $\text{kg s}^{-1} \text{ m}^{-1}$ ) is

$$M(F, z) = 1.8 \rho(z) F^{1/3} z / 4 (\pi/2)^{1/2}.$$

### Example: Stable Stratification

We will assume that the plume structure described above for neutral stratification is valid at levels below the maximum plume height,  $h$ .

1. The total buoyancy flux at the source is that for a fire with a 5-m flame length. Byram's (1959) fire intensity equation is

$$I = 258 \times 10^3 L_f^{2.17},$$

where  $I$  is the fire intensity in  $\text{W/m}$  and  $L_f$  is the flame length in  $\text{m}$ . For  $L_f = 5 \text{ m}$ ,  $I = 8.48 \text{ MW/m}$ . The corresponding total buoyancy flux is

$$F = \frac{g}{\rho c_p \theta_0} I = 230 \text{ m}^3/\text{s}^3,$$

for gravity  $g = 9.81 \text{ m/s}^2$ , air density  $\rho = 1.2 \text{ kg/m}^3$ , specific heat capacity at constant pressure  $c_p = 1004 \text{ J/kg/K}$ , and reference potential temperature  $\theta_0 = 300 \text{ K}$ .

2. A plume can penetrate to a particular height  $h$  that depends on  $F$  and the stability  $N$ :

$$h = 2.85 F^{1/3} N^{-1}.$$

For  $F$  as specified above and  $N = 0.01 \text{ s}^{-1}$ , a typical mid-latitude value,  $h = 1747 \text{ m}$ .

3. The maximum (i.e., centerline) plume updraft speed at any level below  $h$  is  $1.8 F^{1/3}$ . For  $F$  as specified, this speed is  $11.0 \text{ m/s}$ .
4. To construct top hat instead of Gaussian profiles, we must define the plume edge. If we define the edge by a plume threshold updraft speed,  $w_e$ , then the distance of the edge from the plume centerline is

$$R = z \left( \log(1.8 F^{1/3} / w_e) / 32 \right)^{1/2}.$$

For  $w_e = 0.5 \text{ m s}^{-1}$ ,  $z = 1000 \text{ m}$ , and  $F$  as specified,  $R = 311 \text{ m}$ , so the plume is  $622 \text{ m}$  wide.

5. Once the plume edge is specified, average values of vertical velocity and buoyancy within the plume can be calculated using

$$w_p = \frac{\sqrt{\pi} 1.8 F^{1/3} z}{2\sqrt{32} R} \text{erf} \left( \sqrt{32} \frac{R}{z} \right)$$

and

$$b_p = \frac{\sqrt{\pi} 2.6 F^{2/3}}{2\sqrt{41} R} \text{erf} \left( \sqrt{41} \frac{R}{z} \right).$$

For  $F$ ,  $z$ , and  $R$  as specified,  $w_p = 5.5 \text{ m s}^{-1}$  and  $b_p = 0.043 \text{ m s}^{-2}$ .