

# Turbulence Kinetic Energy (TKE) Equation

To study turbulence production we form an eq. for TKE:

- (1) Subtract mean momentum eqs. (for  $\bar{u}, \bar{v}, \bar{w}$ ) from eqs. for  $u, v, w$  to get eqs. for  $u', v', w'$ .
- (2) multiply eqs. for  $u', v', w'$  by  $u', v', w'$  respectively and sum.
- (3) Average the result to get an eq. for  $\overline{u'^2} + \overline{v'^2} + \overline{w'^2}$ , which is  $2 \times$  TKE per unit mass.

The resulting eq. is complicated. It can be written symbolically as:

$$\frac{\overline{D}(\text{TKE})}{Dt} = \underbrace{MP}_{\substack{\text{mechanical} \\ \text{(shear)} \\ \text{production}}} + \underbrace{BPL}_{\substack{\text{buoyant} \\ \text{production} \\ \text{or loss}}} + \underbrace{TR}_{\substack{\text{redist.} \\ \text{by turb.} \\ \text{transport} \\ \text{\& pressure} \\ \text{forces}}} - \underbrace{\epsilon}_{\substack{\text{frictional (viscous)} \\ \text{dissipation} \\ > 0}} \quad (5.14)$$

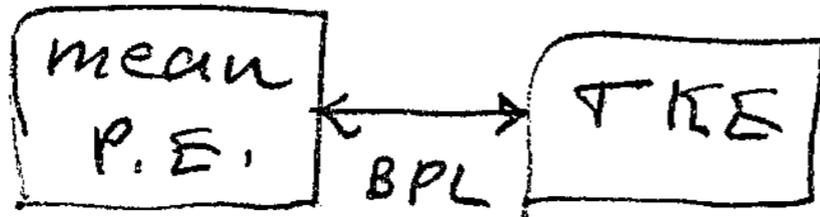
$$\frac{\overline{D}(\text{TKE})}{Dt}$$

$$= \underbrace{MP}_{\text{mechanical (shear) production}} + \underbrace{BPL}_{\text{buoyant production or loss}} + \underbrace{TR}_{\text{redist. by turb. transport \& pressure forces}} - \underbrace{\epsilon}_{\text{frictional (viscous) dissipation}} \quad (5.14)$$

$> 0$

BPL

: conversion between mean flow potential energy and turbulent K.E.



For dry air,  $BPL = \frac{g}{\theta_0} \overline{w'\theta'}$ .

Recall that for a single parcel,

$$\frac{1}{2} (w_2^2 - w_1^2) = \int_{z_1}^{z_2} \frac{g}{\theta_0} \theta' dz,$$

where  $\theta' = \theta - \bar{\theta}$ .

Divide by  $\Delta t = \Delta z / w$ ; where  $\Delta z = z_2 - z_1$ ; and  $w \approx \frac{1}{2}(w_1 + w_2)$ .

$$\frac{\frac{1}{2} (w_2^2 - w_1^2)}{\Delta t} = \frac{w}{\Delta z} \int_{z_1}^{z_1 + \Delta z} \frac{g}{\theta_0} \theta' dz.$$

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By fundamental theorem of calculus, as  $\Delta t, \Delta z \rightarrow 0$ ,

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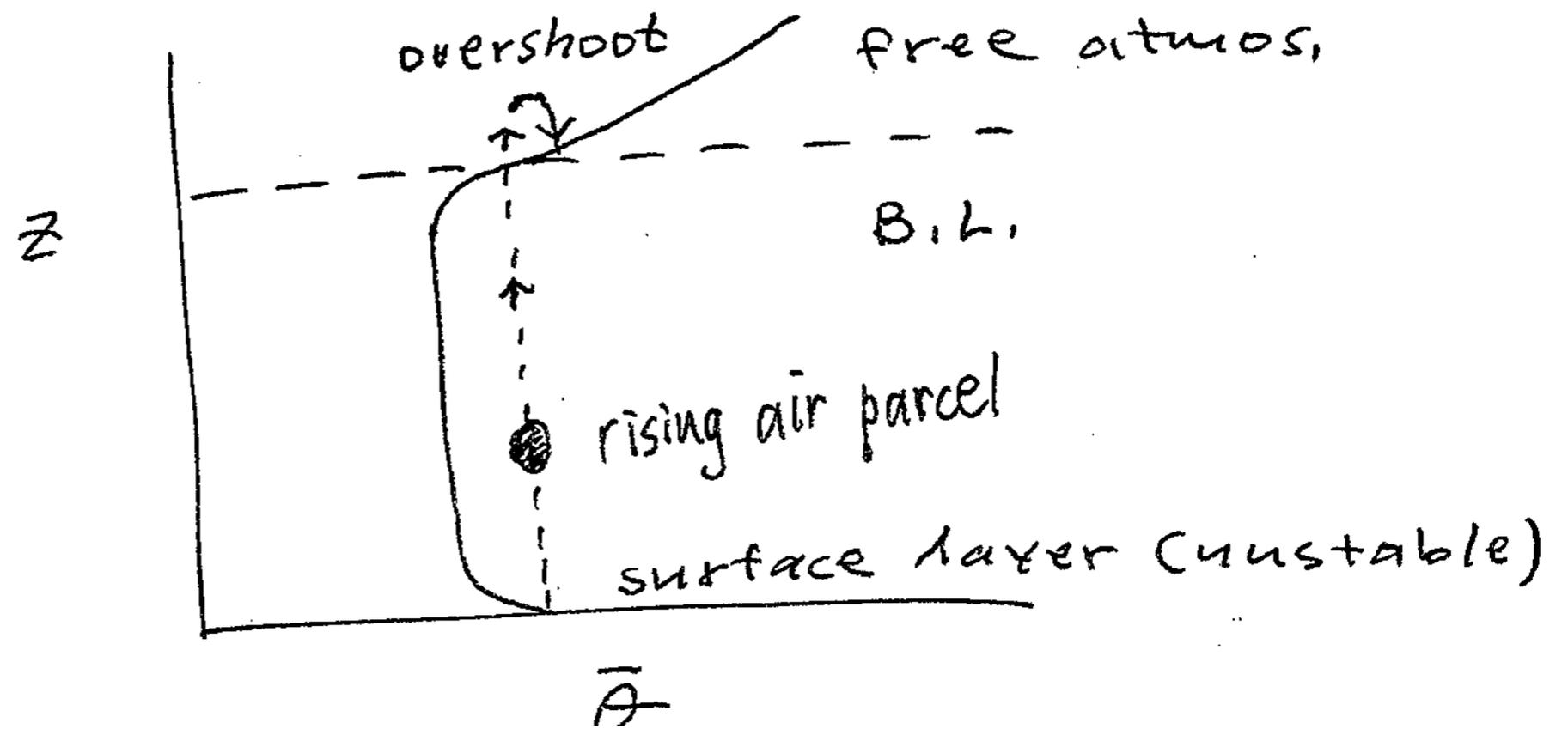
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But  $w = \bar{w} + w'$   $\approx w'$  since  $\bar{w} \approx 0$ , so

$$\boxed{\frac{d}{dt} \left( \frac{w'^2}{2} \right) = \frac{g}{\theta_0} w' \theta'}$$

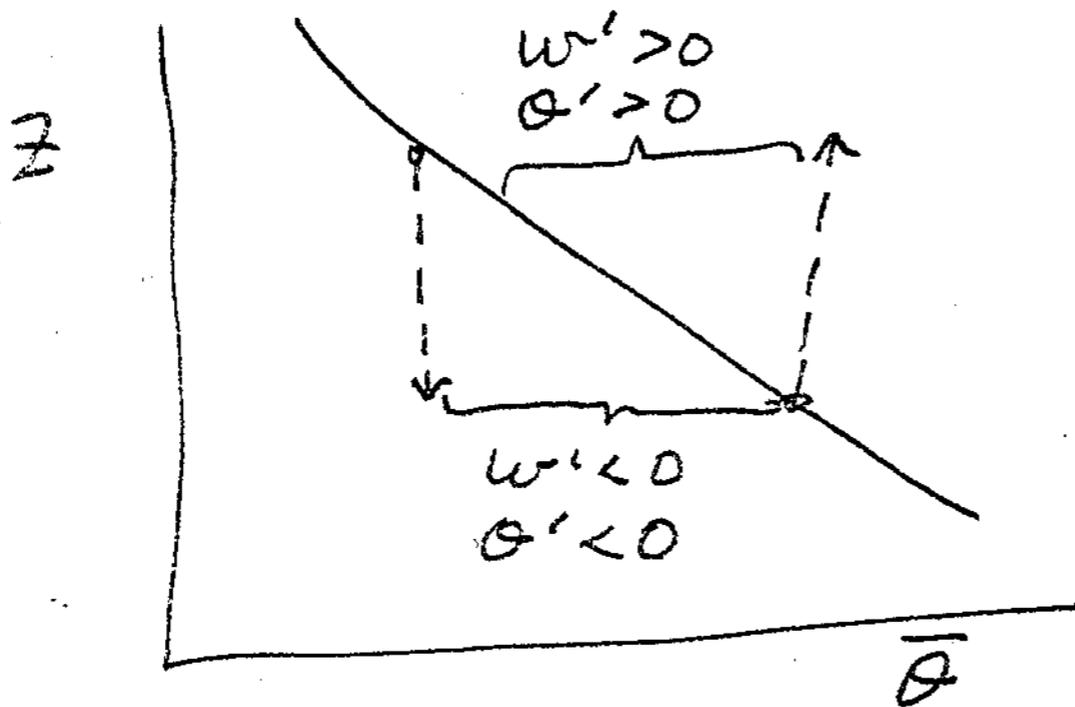
Average to get  $\frac{d}{dt} \left( \overline{\frac{w'^2}{2}} \right) = \frac{g}{\theta_0} \overline{w' \theta'}$ .

Positive Buoyancy prod. occurs when there is heating at surface so an unstable lapse rate develops:

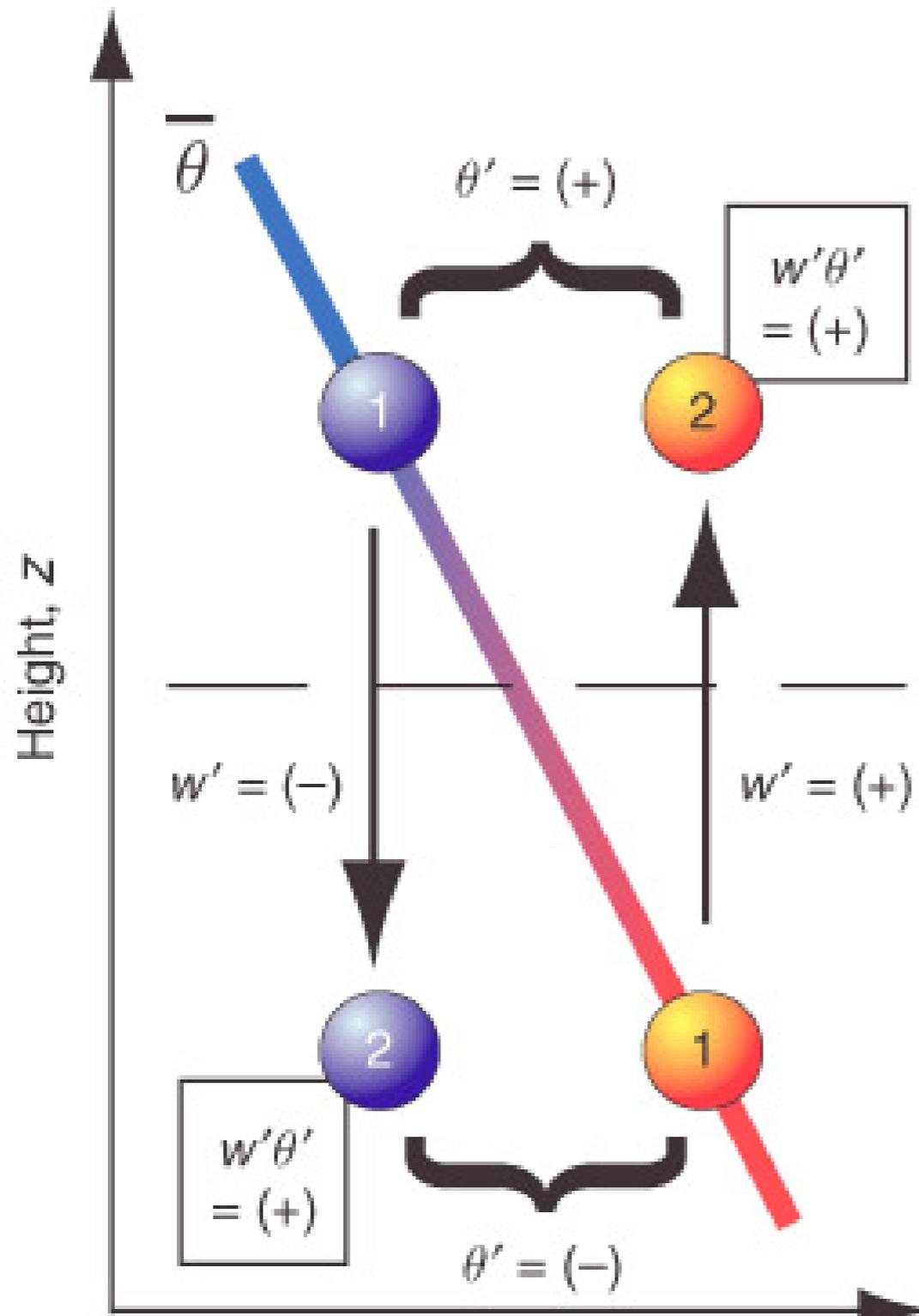


Stull,  
Fig. 16.11

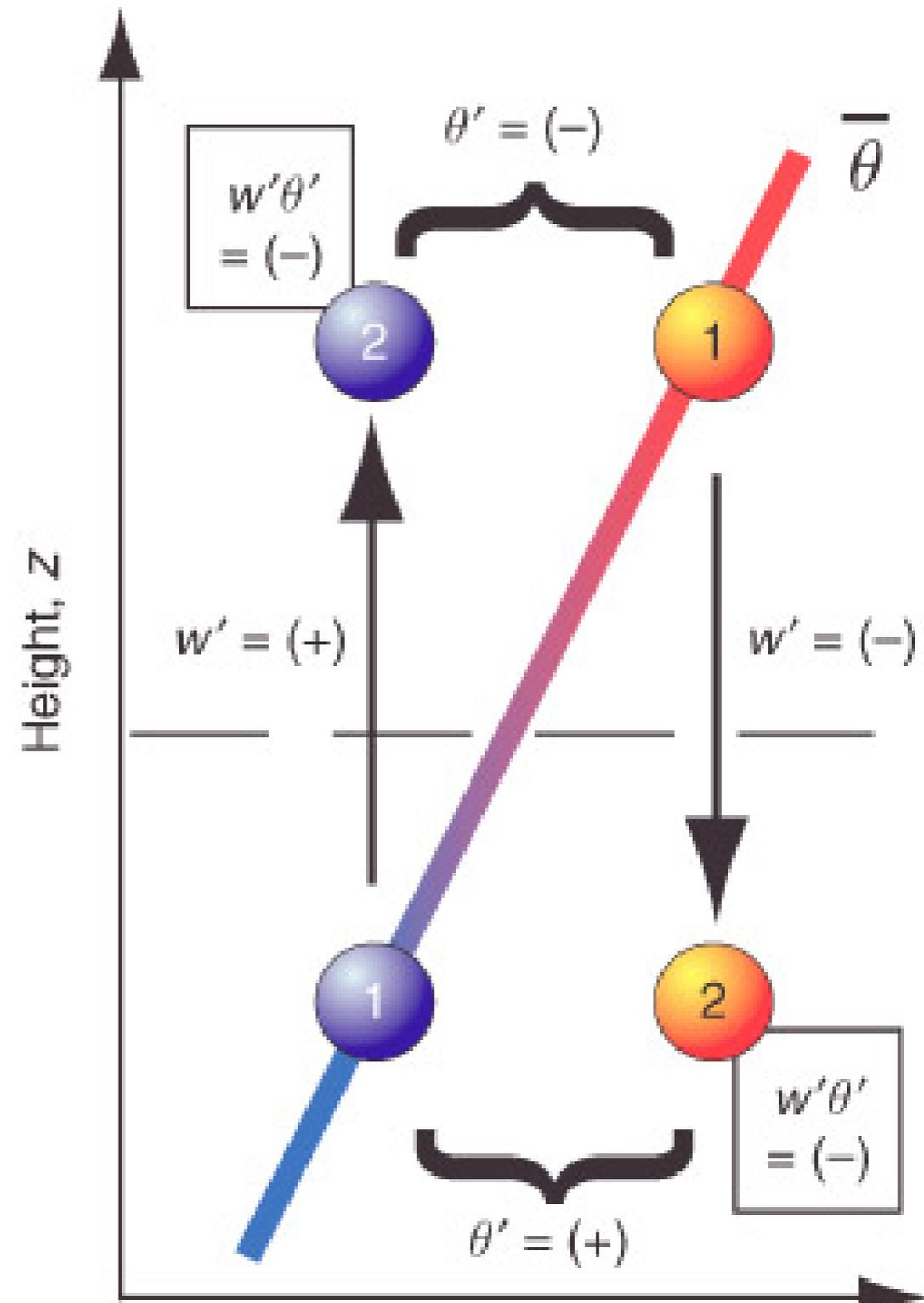
Notice that in surface layer,  $\overline{w'\theta'} > 0$  :



If  $\bar{\theta}$  profile is stable,  $\overline{w'\theta'} < 0$ , which reduces or stops turbulence.



Potential Temperature,  $\theta$   
 (a) Statically unstable:  $\partial\bar{\theta}/\partial z < 0$ .



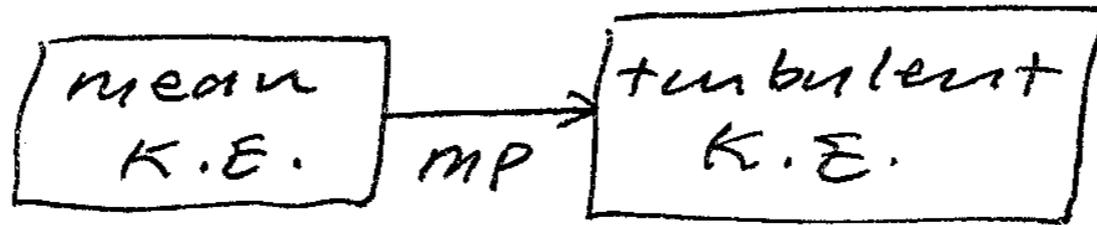
Potential Temperature,  $\theta$   
 (b) Statically stable:  $\partial\bar{\theta}/\partial z > 0$ .

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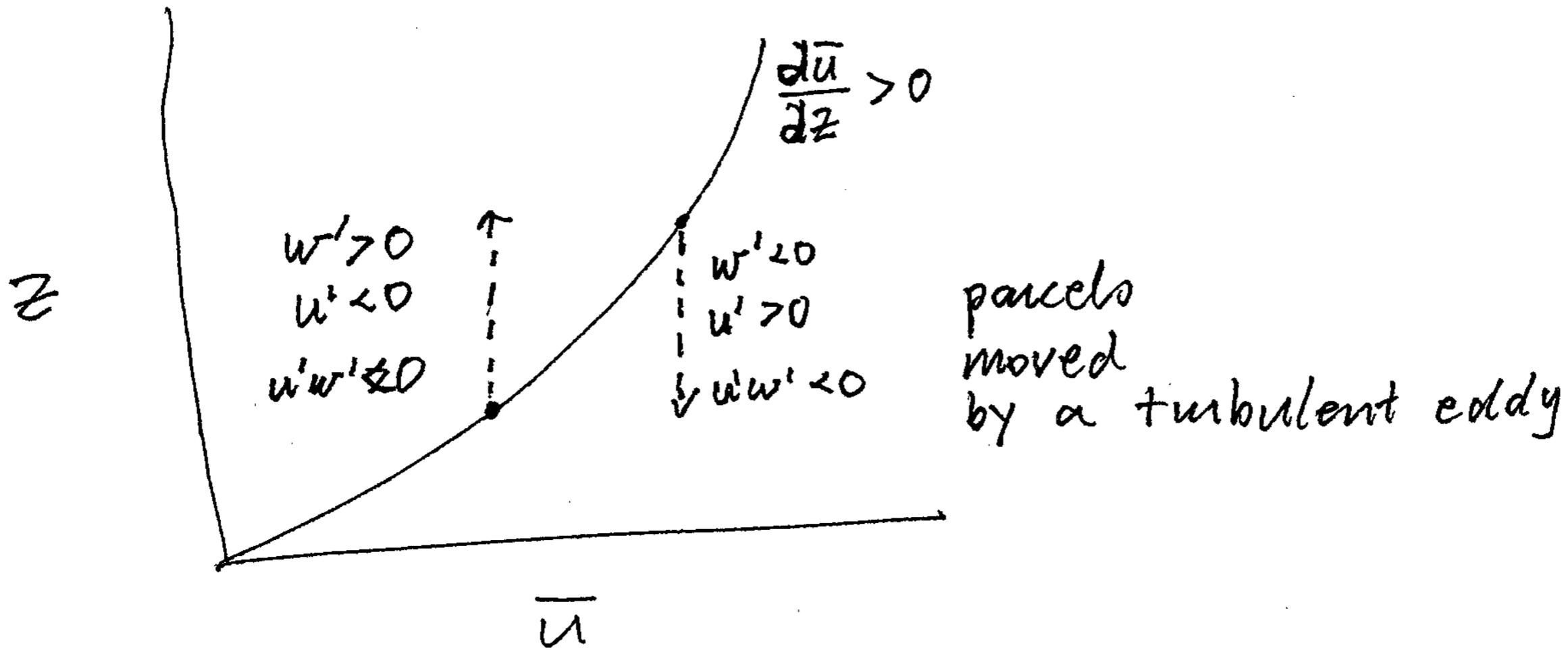
MP :



$$MP = \underbrace{-\overline{u'w'}}_{\text{shear}} \frac{\partial \bar{u}}{\partial z} - \overline{v'w'} \frac{\partial \bar{v}}{\partial z}$$

(MP > 0 when momentum flux is down gradient of mean momentum.)

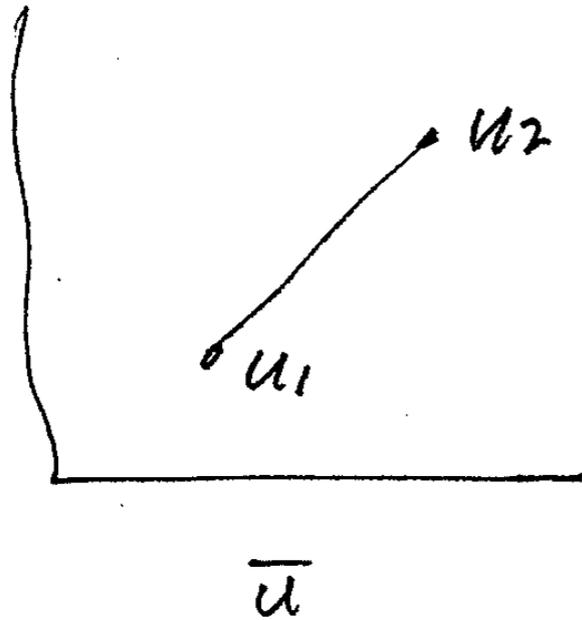
# Mechanical (Shear) Production (MP)



momentum is transferred from region of large  $\bar{u}$  to region of low  $\bar{u}$ , i.e., down gradient, while  $\overline{u'w'} < 0$  and  $MP > 0$ .

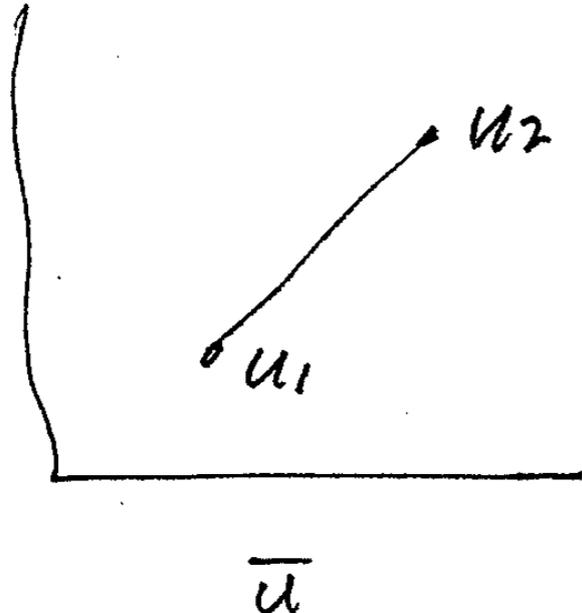
# Effect of MP on mean wind profile and mean KE

before turbulence

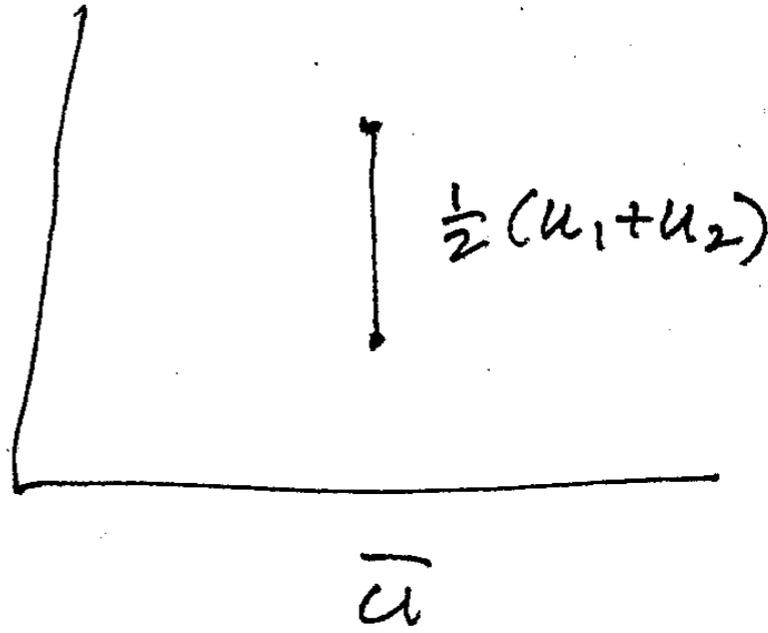


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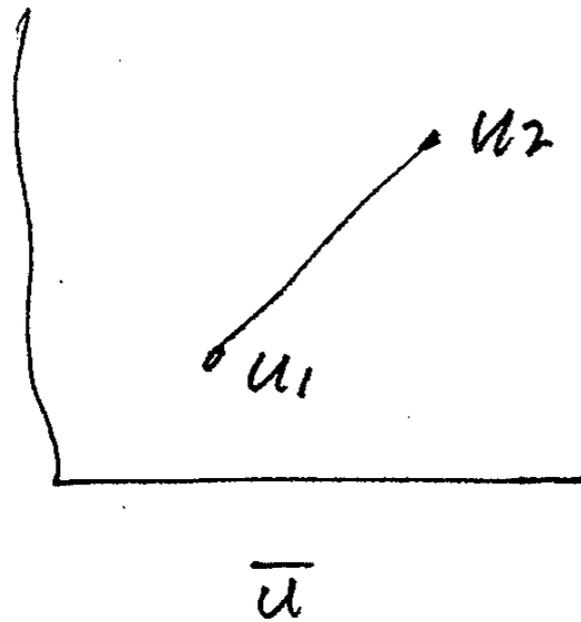


after turbulence

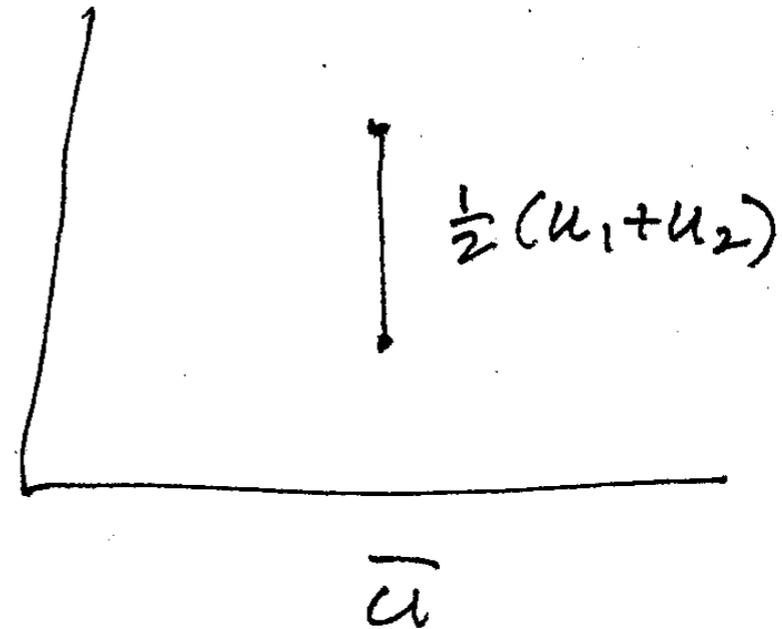


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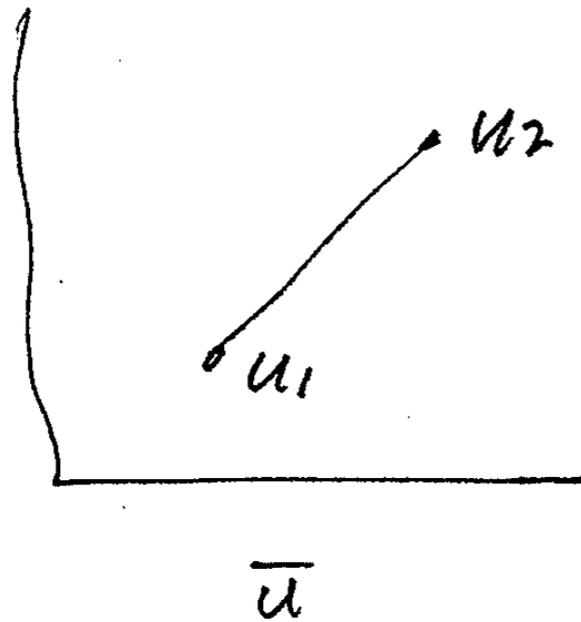
mean K.E. for layer =

$$\frac{1}{2} (u_1^2 + u_2^2)$$

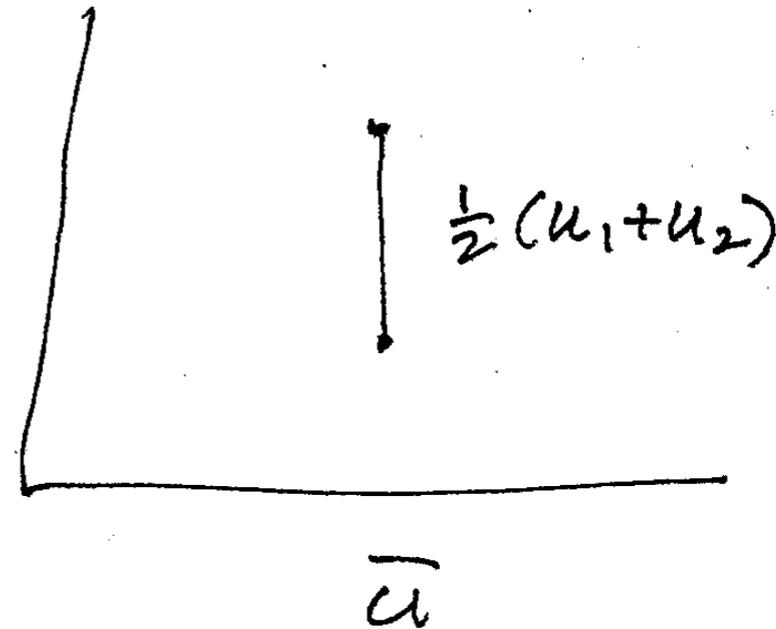
**BEFORE**

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$$2 \times \frac{1}{2} \left[ \frac{1}{2} (u_1 + u_2) \right]^2 \\ = \frac{1}{2} [u_1^2 + u_2^2 + 2u_1u_2]$$

**AFTER**

# Effect of MP on mean wind profile and mean KE

What is change in mean K.E. for layer?  
Before - After =

$$\begin{aligned}\frac{1}{2}(u_1^2 + u_2^2) - \left[\frac{1}{2}(u_1 + u_2)\right]^2 &= \frac{u_1^2}{2} + \frac{u_2^2}{2} - \frac{u_1^2}{4} - \frac{u_2^2}{4} - \frac{u_1 u_2}{2} \\ &= \frac{u_1^2}{4} + \frac{u_2^2}{4} - \frac{u_1 u_2}{2} \\ &= \frac{1}{4}(u_1^2 + u_2^2 - 2u_1 u_2) \\ &= \frac{1}{4}(u_1 - u_2)^2.\end{aligned}$$

Thus, regardless of sign of  $u_1 - u_2$ , mean K.E. decreases due to mixing by turbulence.

# Static Stability, TKE, and Richardson Number

If layer is statically stable, can turbulence exist? only if  $MP$  is large enough:

(as measured by flux Richardson number)

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- As static stability increases, depth of turbulent layer decreases.

# Static Stability, TKE, and Richardson Number

At night, a strong temperature inversion may be produced by radiative cooling of the surface, and the BL depth may be only a few <sup>(decameters)</sup> dm deep, since turbulence is suppressed at higher levels where  $MP$  is small and  $BPL \leq 0$ .

