

Stable case ($N^2 = \text{constant} > 0$); can solve set analytically.

2. As before, use new variables:

$$M \equiv R^3 w, \quad V \equiv R^3, \quad F \equiv R^3 B.$$

At $t = 0$: $M = V = 0, \quad F = F_0 (= \frac{3Q}{4\pi}),$

where

$$Q \equiv \oint B_0 d\tau.$$

3. Render dimensionless (the resulting eqs.)

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$$\begin{aligned} F^* &= F_0 f && * \text{ dimensional} \\ M^* &= \frac{3}{4\pi} F_0 N^{-1} m \\ V^* &= \left(\frac{3}{\pi}\right)^{3/4} \alpha^{3/4} F_0^{3/4} N^{-3/2} v \\ t^* &= N^{-1} t. \end{aligned}$$

Obtain dimensionless forms of gov. eqs. (see text, Eqs. (2.7.19) - (2.7.21)).

Can get h.t. of thermal from $\int dz/dt = w$.
Scale z :

$$\frac{M^*}{V^*} t^* = z^* = \frac{1}{4} \left(\frac{3}{\pi}\right)^{1/4} \alpha^{-3/4} F_0^{1/4} N^{-1/2} z$$

$$= w^* t^*$$

Recall that $w^* = M^*/V^*$, so $w = m/v$ (non-dim.),
as expected,

$$\frac{dz}{dt} = \frac{m}{v} \text{ (non-dim.)} \quad (2.7.22)$$

4. Apply b.c.s to solve

Sols. for R, w, B are obtained, with new b.c.s, sequentially for each segment of upward and downward motion, i.e., for $0 \leq t \leq \pi$ (non-dim.):

$$z = 4(1 - \cos t)^{1/4}$$

(see text for others.)

- * See Fig. 2.8 Damped oscillatory motion. max. (dimensionless) ht. of 4.75, eventually asymptotes to 4.2.

Sec 2.8 Experiments and observations

- * Show Fig. 2.9 - plumes in neutral & stable stratif.
- * Show Fig. 2.10 - plume in stable stratif, shows expected dependence on $Fo^{1/4} N^{-3/4}$ of plume ht.
- * Show Fig. 2.11 - Thermal max. ht. in stable stratif. Shows expected dependence on $Fo^{1/4} N^{-1/2}$
- * Show Fig. 2.12 Shape preservation of thermal in neutral enviro.
- * Fig. 2.15 z^2 vs t shows expected linear relationship deduced from dim. anal.
- * Fig. 2.16 circulation within a thermal & "spherical vortex."

H.W. - Do exercises 2.1-2.4
For 2.3, use $d = 0.093$.

2.8 Experiments and observations

In analytic solutions, as well as numerical ones, α remained an undetermined constant, to be somehow determined from experiment.

For alternate approach (p. 5)

Plumes in a stable stratification can be used because the lower part of the plume is essentially the same as that of a similar plume when $N^2 = 0$, (see Fig. 2.7).

2.9

From measured heights of a plume in a stable stratification plotted vs. $F_0^{1/4} N^{-3/4}$, as in Fig. 2.10, we can determine the constant α , since we saw in §2.7 that h_t depends only on α , F_0 , and N .

Specifically, for a plume,

$$Z^* = 0.410 \alpha^{-1/2} F_0^{1/4} N^{-3/4} Z \quad (\text{p. 30})$$
 where Z is the ^{n.d.} h_t of some feature, such as max. plume h_t , and Z^* is dimensional h_t (measured).

We found that $Z = 2.8$ at plume top, so

$$Z^* / (F_0^{1/4} N^{-3/4}) = 0.410 \alpha^{-1/2} (2.8).$$
 Actual slope is 3.79, so $\alpha = \frac{3.79}{2.8 \times 0.410}$

$$\alpha = \left(\frac{2.8 \times 0.410}{3.79} \right)^2 = 0.092.$$

Similarly, for a thermal,

$$Z^* = \frac{1}{4} \left(\frac{3}{\pi} \right)^{1/4} \alpha^{-3/4} F_0^{1/4} N^{-1/2} Z \quad (\text{p. 33})$$

Ultimate n.d. ht. is $z = 4.2$. For z^* vs. $F_0^{1/4} N^{-1/2}$,
 Slope = $\frac{1}{4} \left(\frac{3}{\pi}\right)^{1/4} \alpha^{-3/4} (4.2) = 2.66$ from exp.
 (Fig. 2.11), so $\alpha^{-3/4} = 2.66 / \left(\frac{1}{4} \left(\frac{3}{\pi}\right)^{1/4} 4.2\right) = 2.5627$
 $\alpha = (2.5627)^{-4/3} = 0.285$.

Alternate approach for plume to derive α :

Assume a radial profile of $\exp(-pr^2/z^2)$.

Then slope of ht. of plume top vs. $F_0^{1/4} N^{-3/4}$ depends on p , (see Fig. 2.10),
 Determine p experimentally as best fit to measurements.

Relate p to α as follows:

Equate assumed radial dependence,
 $\exp(-r^2/R^2)$
 to
 $\exp(-pr^2/z^2)$.

Then

$$\frac{R}{z} = p^{-1/2} = \frac{6}{5} \alpha$$

according to solution for plumes with $N^2 = 0$.
 (See discussion on p. 4 for why we can apply this result to stable stratification.)

From Fig. 2.10, $p = 80$ is best ~~choice~~ match.

Then $d = \frac{5}{6} p^{-1/2} = \frac{5}{6} (80)^{-1/2} = \underline{0.093}$.