# LES of Turbulent Flows: Lecture 9 (ME EN 7960-008)

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#### **Eddy viscosity Models**

- **Eddy Viscosity Models:** (Guerts pg 225; Pope pg 587)
  - -In Lecture 8 we said an eddy-viscosity models are of the form:

momentum:  $\tau_{ij} = -2\nu_T \tilde{S}_{ij} \end{red} \mbox{filtered strain rate}$  eddy-viscosity

scalars:  $q_i = -D_T \frac{\partial \tilde{\theta}}{\partial x_i} \text{ where } D_T = \frac{\nu_T}{Pr_{sgs}} \text{ SGS Prandtl number}$  eddy-diffusivity

- -This is the LES equivalent to 1<sup>st</sup> order RANS closure (k-theory or gradient transport theory) and is an analogy to molecular viscosity (see Pope Ch. 10 for a review)
- -Turbulent fluxes are assumed to be proportional to the local velocity or scalar gradients
- -In LES this is the assumption that stress is proportional to strain:  $\, au_{ij}\sim \hat{S}_{ij}$
- -The SGS eddy-viscosity  $\nu_T$  must still be parameterized.

#### **Eddy viscosity Models**

-Dimensionally =>

$$\nu_T = \left\lceil \frac{L^2}{T} \right\rceil$$

-In almost all SGS eddy-viscosity models  $\, \nu_T \sim u^* l^* \,$  velocity scale velocity scale

- -Different models use different  $u^*$  and  $l^*$
- -Recall the filtered N-S equations:

$$\frac{\partial \tilde{u}_i}{\partial t} + \frac{\partial \tilde{u}_i \tilde{u}_j}{\partial x_j} = -\frac{\partial \tilde{p}}{\partial x_i} + \frac{1}{Re} \frac{\partial^2 \tilde{u}_i}{\partial x_j^2} - \frac{\partial \tau_{ij}}{\partial x_j} + F_i$$

-Note, for an eddy-viscosity model we can write the viscous and SGS stress terms as:

$$\frac{1}{Re} \frac{\partial}{\partial x_i} \tilde{S}_{ij} \text{ and } \tau_{ij} = -2\nu_T \tilde{S}_{ij}$$

We can combine these two and come up with a new (approximate) viscous term:

$$\frac{\partial}{\partial x_j} \left[ \left( \nu_T + \frac{1}{Re} \right) \tilde{S}_{ij} \right]$$

What does the model do? We can see it effectively lowers the Reynolds number of the flow and for high Re (when 1/Re=>0), it provides all of the energy dissipation.

#### Smagorinsky Model

- •Smagorinsky model: (Smagorinsky, MWR 1963)
  - -One of the 1st and still most popular  $\nu_T$  models for LES
  - -Originally developed for general circulation models (large-scale atmospheric), the model did not remove enough energy in this context.
  - -Applied by Deardorff (JFM, 1970) in the 1<sup>st</sup> LES.
  - -Uses Prandtl's mixing length (see Pope Ch. 10 for a review of mixing length) applied at  $\nu_T = \left(C_S \Delta\right)^2 |\tilde{S}|$  length scale velocity scale the SGSs:

-Where  $\Delta$  is the grid scale taken as  $\Delta=(\Delta_x\Delta_y\Delta_z)^{\frac{1}{3}}$  (Deardorff, 1970 or see Scotti et al., PofF 1993 for a more general description).

 $-| ilde{S}|=\sqrt{2 ilde{S}_{ij} ilde{S}_{ij}}$  is the magnitude of the filtered strain rate tensor with units [1/T] and serves as the velocity scale (think  $rac{\partial\langle u
angle}{\partial z}$  in k-theory) and  $C_S\Delta$  is our length scale (squared for dimensional consistency).

-The final model is:

$$\tau_{ij} - \frac{1}{3}\tau_{kk}\delta_{ij} = -2\left(C_S\Delta\right)^2 |\tilde{S}|\tilde{S}_{ij}|$$

-To close the model we need a value of  $C_s$  (usually called the Smagorinsky or Smagorinsky-Lilly coefficient)

## Lilly's Determination of $C_s$

- Lilly proposed a method to determine  $C_s$  (IBM Symposium, 1967, see Pope page 587)
- Assume we have a high-Re flow  $\Rightarrow$   $\Delta$  can be taken to be in the inertial subrange of turbulence.
- The mean energy transfer across  $\Delta$  must be balanced by viscous dissipation, on average (note for  $\Delta$  in the inertial subrange this is not an assumption).

$$\epsilon = \langle \Pi \rangle$$
 recall:  $\Pi = -\tau_{ij} \tilde{S}_{ij}$ 

- -Using an eddy-viscosity model  $u_T \Rightarrow \Pi = 2\nu_T \tilde{S}_{ij} \tilde{S}_{ij} = \nu_T |\tilde{S}|^2$
- -If we use the Smagorinsky model:  $\, 
  u_T = \left( C_S \Delta \right)^2 | ilde{S}| \,$

$$\Rightarrow \qquad \Pi = \left( C_S \Delta \right)^2 |\tilde{S}|^3$$

-The square of  $|\tilde{S}|$  can be written as (see Pope pg 579 for details):

$$|\tilde{S}|^2 = 2 \int_0^\infty k^2 \hat{G}(k)^2 E(k) dk$$
 energy spectrum filter transfer function

- -Recall, for a Kolmogorov spectrum in the inertial subrange  $E(k) \sim C_k \epsilon^{2/3} k^{-5/3}$
- -We can use this in our integral to obtain (see Pope pg. 579):  $|\tilde{S}|^2 \approx a_f C_k \epsilon^{2/3} \Delta^{-4/3}$

### Lilly's Determination of $C_s$

- We can rearrange  $|\tilde{S}|^2 \approx a_f C_k \epsilon^{2/3} \Delta^{-4/3}$  to get:  $\epsilon = \left\lceil \frac{\langle |\tilde{S}|^2 \rangle}{a_f C_k \Delta^{-4/3}} \right\rceil^{\frac{1}{2}}$  (\*)
- ullet Equating viscous dissipation and the average Smagorinsky SGS dissipation (  $\epsilon = \langle \Pi 
  angle$  ):

$$\epsilon = \langle \left( C_S \Delta \right)^2 | \tilde{S} |^3 \rangle$$

• if we now combine this equation with (\*) above and do some algebra...

$$C_S = \frac{1}{\left(C_k a_f\right)^{3/4}} \left(\frac{\langle |\tilde{S}|^3 \rangle}{\langle |\tilde{S}|^2 \rangle^{3/2}}\right)^{-\frac{1}{2}}$$

• we can use the approximation  $\langle |\tilde{S}|^3 \rangle \approx \langle |\tilde{S}|^2 \rangle^{3/2}$  and  $a_f$  for a cutoff filter (see Pope)

$$\Rightarrow C_S = \frac{1}{\pi} \left( \frac{2}{3C_k} \right)^{3/4}$$

•  $C_k$  is the Kolmogorov constant ( $C_k \approx 1.5$ -1.6) and with this value we get:

$$C_{\rm S}$$
 ≈ 0.17